

# Unstructured Grids for Sonic Boom Analysis and Design

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# Outline

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- Background
- Description of methods
  - Cylindrical Outer Boundary (COB)
  - Boom Grid (BG)
  - Near-Field Target (NFTARG)
- Results
  - Parametric grid generation studies
  - Exploratory design cases
- Concluding remarks

# Technology Challenge Goals



| Balanced Goals for Practical Civil Supersonic Aircraft (Technology Available) | N+1 Supersonic Business Class Aircraft (2015) | N+2 Small Supersonic Airliner (2020) | N+3 Efficient Multi-Mach Aircraft (Beyond 2030)               |
|---|---|--------------------------------------|---|
| <b>Design Goals</b>   |   |                                      |   |
| Cruise Speed  | Mach 1.6-1.8                                  | Mach 1.6-1.8                         | Mach 1.3-2.0  |
| Range (n.mi.)   | 4000  | 4000                                 | 4000 - 5500   |
| Payload (Passengers)  | 6 - 20  | 35 - 70                              | 100 - 200   |
| <b>Environmental Goals</b>  |   |                                      |   |
| Sonic Boom  | 65 - 70 PLdB                                  | 85 PLdB (Revised)                    | 65 - 70 PLdB Low Boom Flight<br>75 - 80 PLdB Overwater Flight |
| Airport Noise (cumulative below stage 4)                                      | Meet with Margin                              | 10 EPNdB                             | 10 - 20 EPNdB   |
| Cruise Emissions (Cruise Nox g/kg of fuel)                                    | Equivalent to current Subsonic                | < 10                                 | < 5 & particulate and water vapor mitigation                  |
| <b>Efficiency Goals</b>   |   |                                      |   |
| Fuel Efficiency (passenger miles per lb of fuel)                              | 1.0   | 3.0                                  | 3.5 - 4.5   |

- NASA defined an initial set of design parameters and performance levels for practical supersonic airliners in the near, mid and far term time frames
- Systems Studies have been used to determine if these goals are valid and achievable

N+1 Business Class



N+2 Small Supersonic Airliner



N+3 Efficient, Multi Mach Aircraft



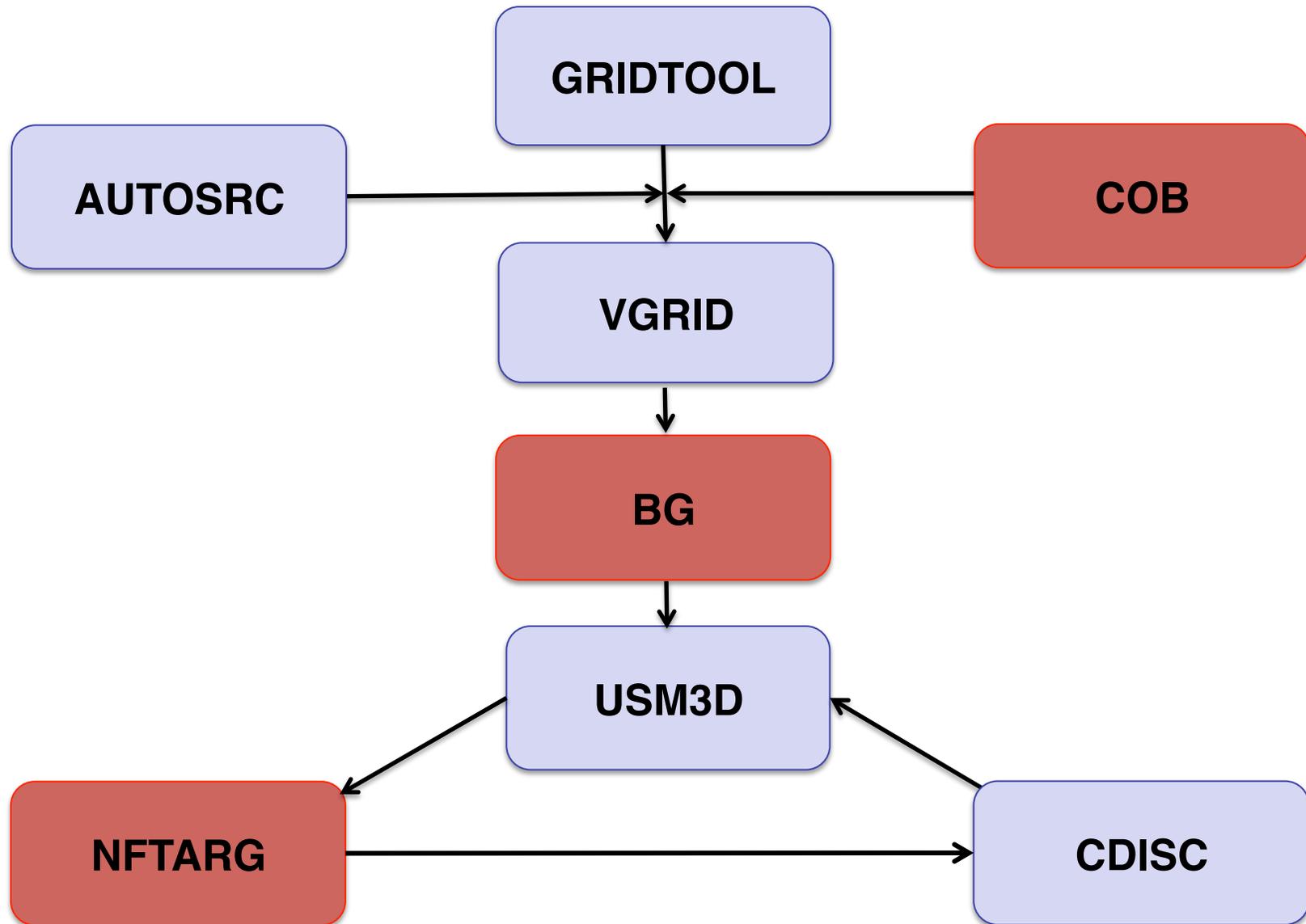
# Recent Sonic Boom Research Using CFD Analysis and Design

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- Shaped Sonic Boom Demonstration (flight tests, 2005)
- Gulfstream Quiet Spike test program (flight tests, 2008)
- NASA Sonic Boom Workshop (2008)
- NRA N+2 Studies (CFD and WT tests, 2013)
  - Boeing
  - Lockheed
- AIAA 1<sup>st</sup> Sonic Boom Prediction Workshop (2014)
- NASA Sonic Boom Unstructured Grid Generation
  - Stretched: SSGRID, SSGN
  - Extrusion: MCAP, **BG**, INFLATE
  - Adaptive: FUN3D

# Flow Chart of Sonic Boom Analysis and Design Process Using TetrUSS



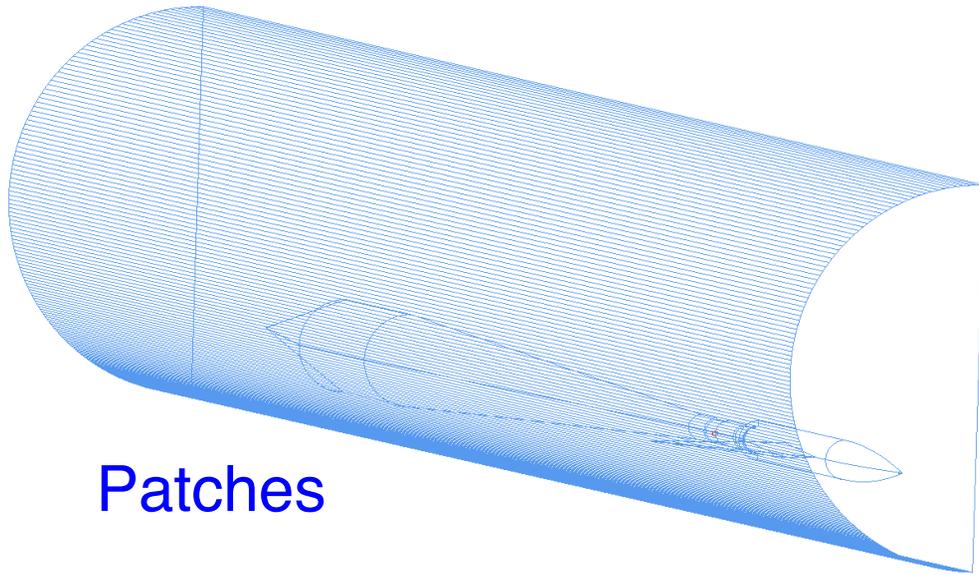
# Core Grid Generation Codes

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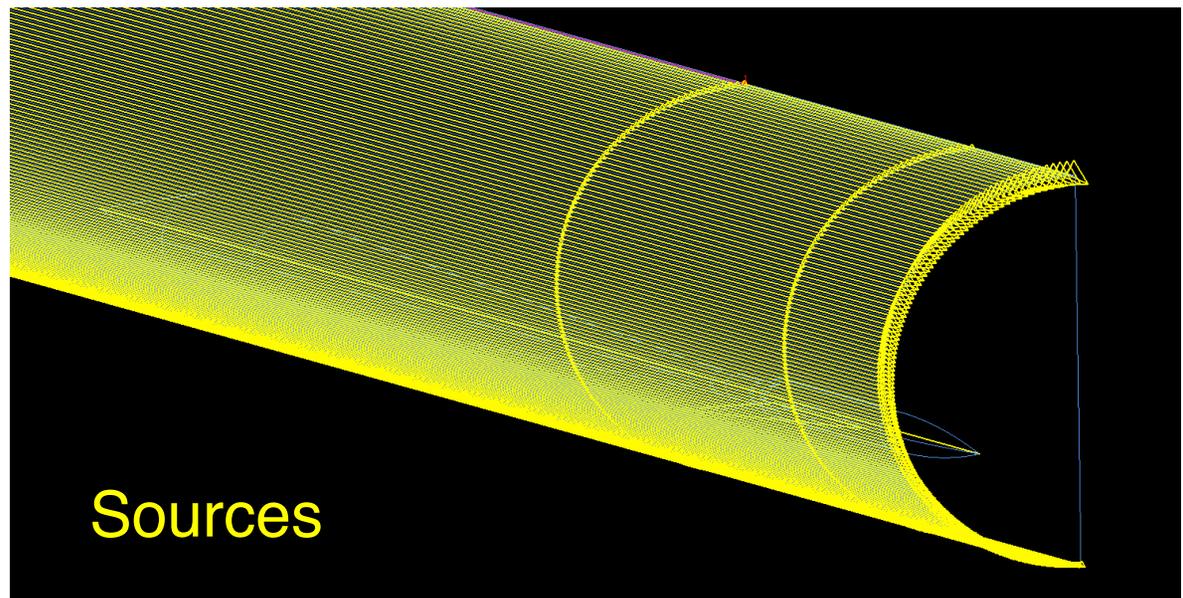


- Configuration setup
  - **GRIDTOOL**: define surface curves and patches from IGES or other geometry definition formats
  - **AUTOSRC**: automatically locate and size line sources that control surface grid spacing based on aircraft component type
- Outer boundary setup
  - **COB**: define curves, patches and sources for cylindrical or rectangular outer boundary for robust BG extrusion process
- Core grid generation
  - **VGRID**: generate body-fitted tetrahedral core grid using advancing layer and advancing front methods

# COB Cylindrical Outer Boundary

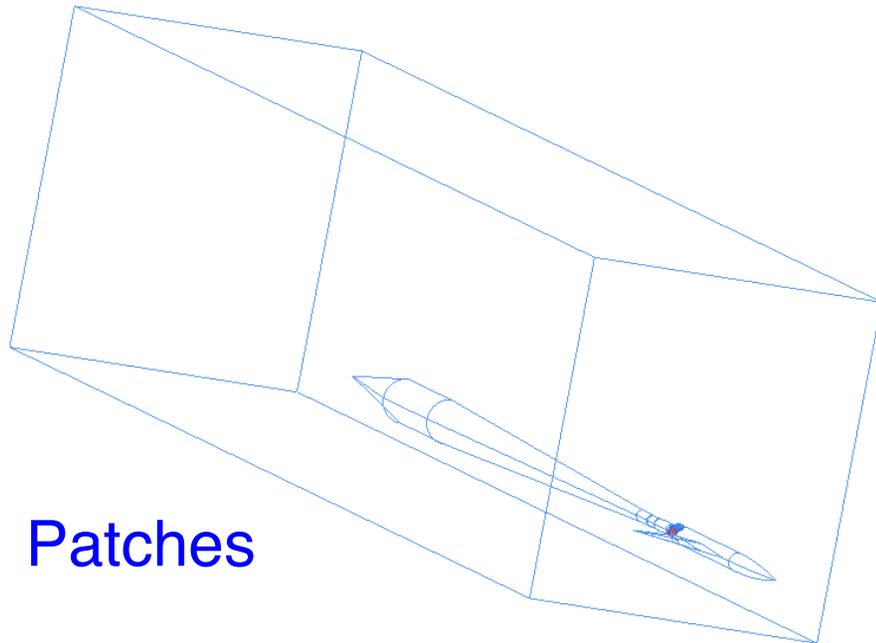


Patches

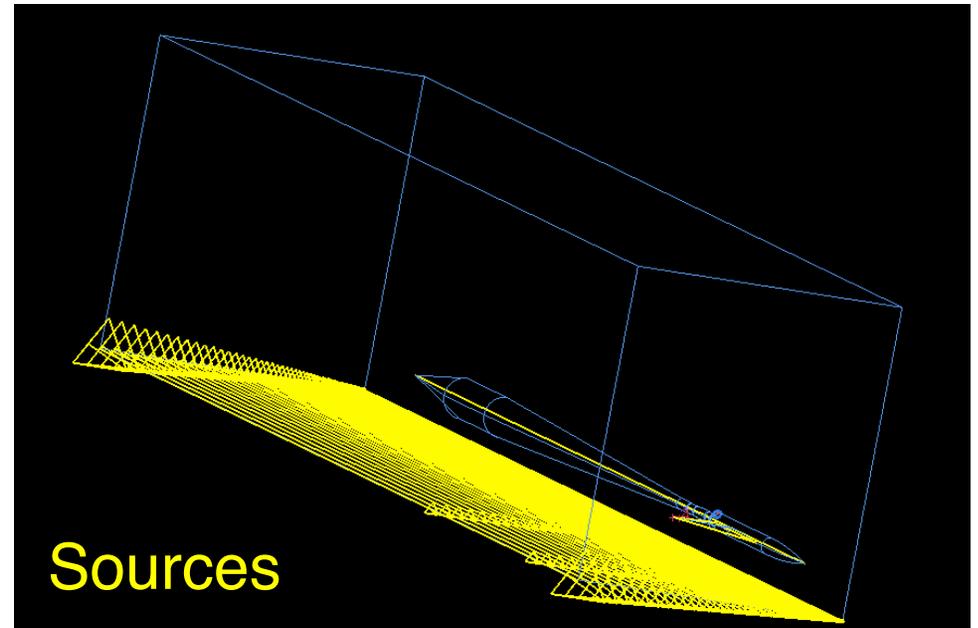


Sources

# COB Rectangular Outer Boundary

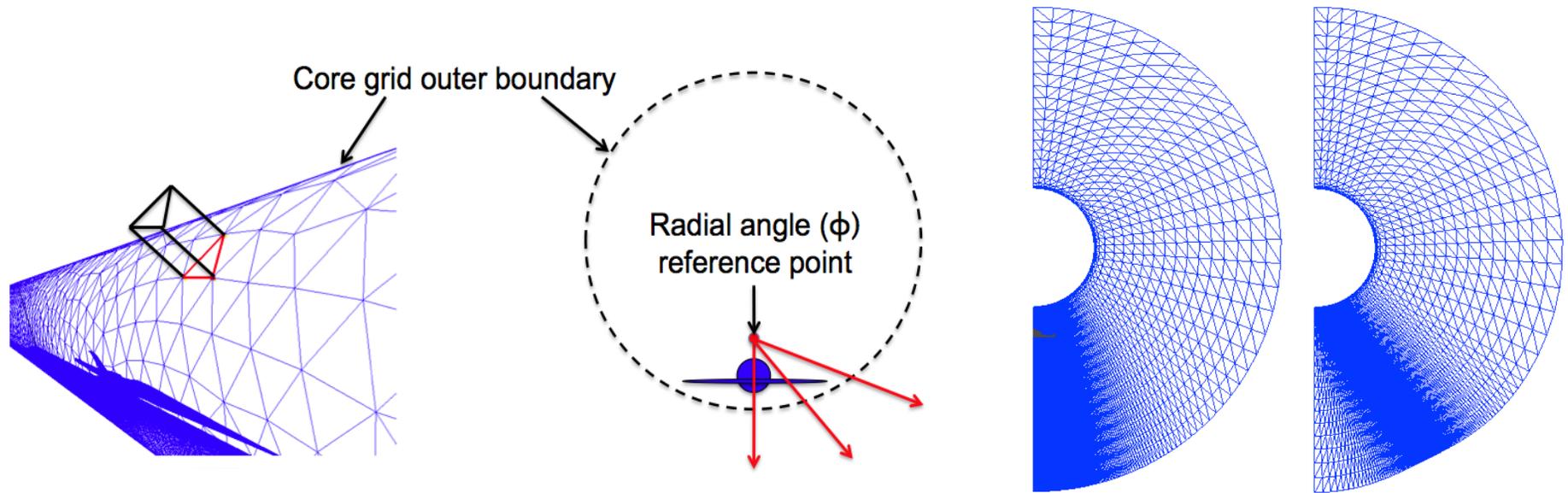


Patches



Sources

# BG Collar Grid Generation Code



- Extrude layers of prisms through faces on core grid outer boundary
- Split prisms into tetrahedral cells and merge with core grid
- Radial angle reference point for extrusion located close to configuration nose
- Vary height of reference point to focus grid at selected radial angles

# Analysis and Design Codes

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- Flow solver – **USM3D**
  - Solves RANS equations using a cell-centered, upwind scheme
  - SST turbulence model used for viscous cases
  - Minmod limiter used for solution stability for all cases
- Target Pressure Generation – **NFTARG**
  - Ray-tracing method to link surface geometry to near-field target
  - Several options available for target specification
- Design module – **CDISC**
  - Knowledge-based design to target pressure distribution
  - Prescribed flow/geometry sensitivity derivatives
  - Flow constraints automatically generate target pressures
  - Geometry constraints incorporate multidisciplinary influences

# Configurations Used in Code Evaluation Studies

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Body of revolution (SEEB) - Euler



Delta wing-body (DWB) - Euler



Full aircraft (LM1021) - RANS



# Summary of Parametric Grid Generation Studies - COB

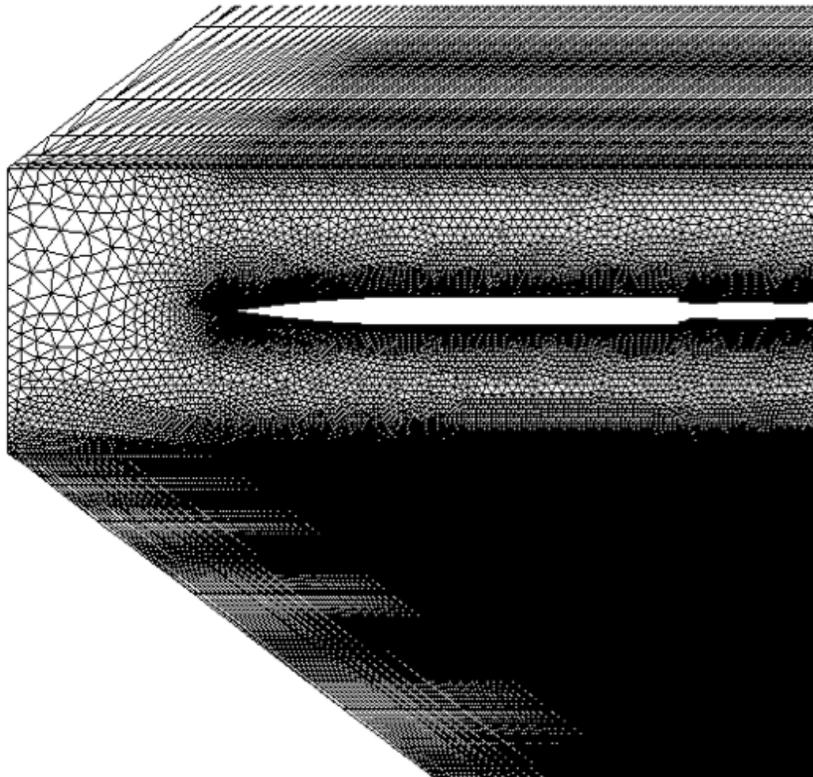


| <u>Parameter</u>            | <u>Configuration</u> | <u>Range</u>  | <u>Significant</u> |
|-----------------------------|----------------------|---------------|--------------------|
| Core grid vertical location | DWB                  | center, low   | yes                |
| Axial spacing parameter     | DWB                  | 100 – 500     | yes                |
| Multi-zone axial spacing    | DWB                  | 3,4 zones     | yes                |
| Off-track enhancements      | DWB                  | 0, 30, 60 deg | no                 |
|                             | LM1021               | 0, 50 deg     | no                 |
| Outer boundary shape        | DWB                  | cyl, rec      | yes                |

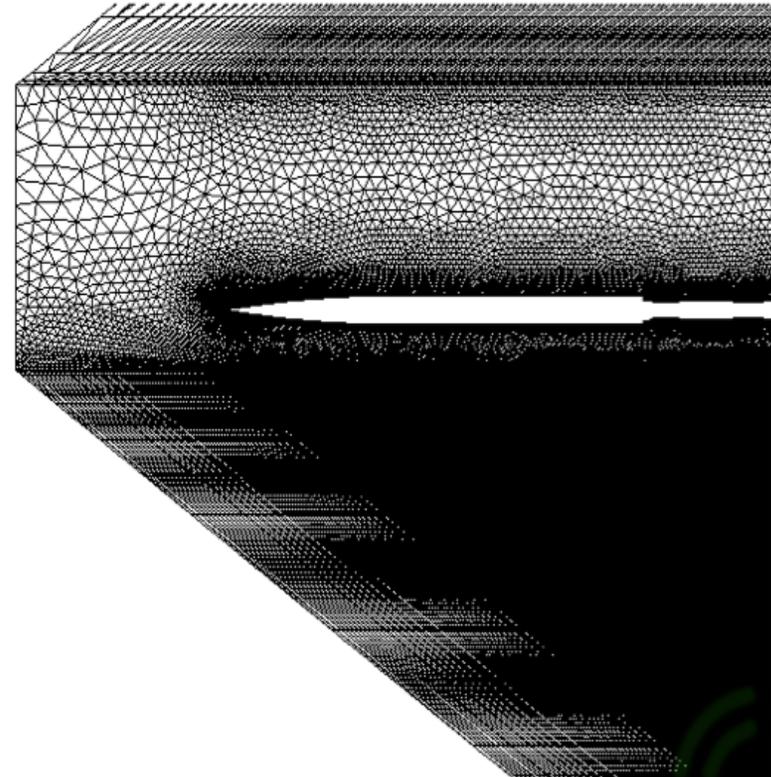
# Symmetry Plane Grids for Different Core Grid Vertical Locations



Core grid centered  
at model nose



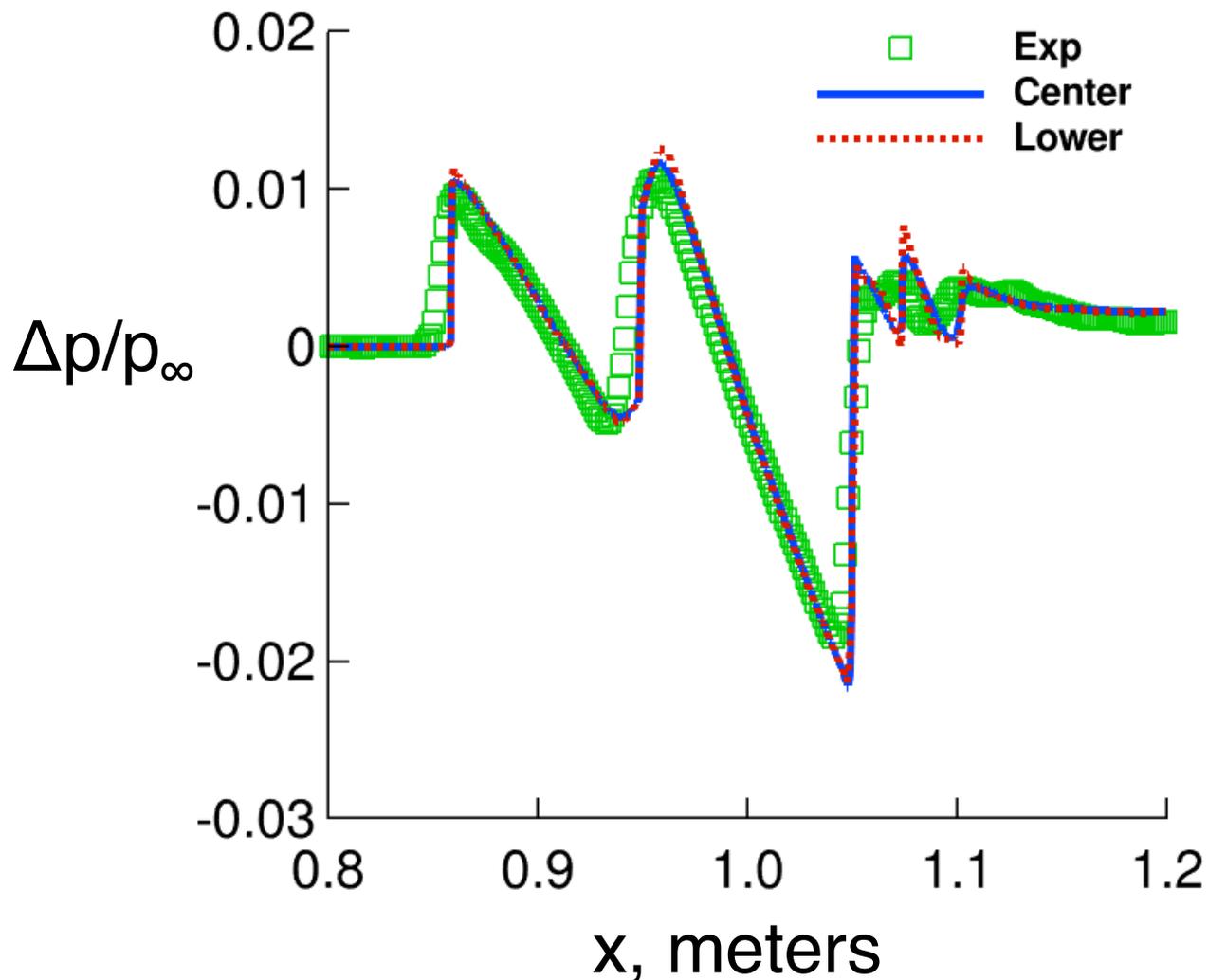
Core grid automatically  
positioned by COB



# Effect of Core Grid Vertical Location on DWB Near-field Boom Signature



$M = 1.7$     $H/L = 3.6$     $\Phi = 0$  deg

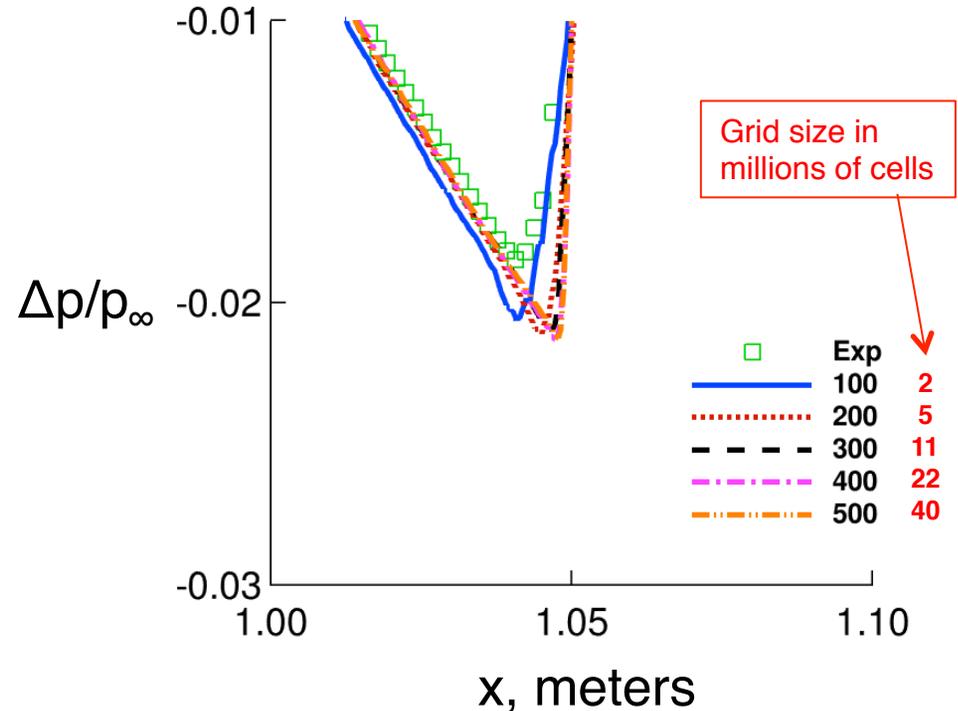
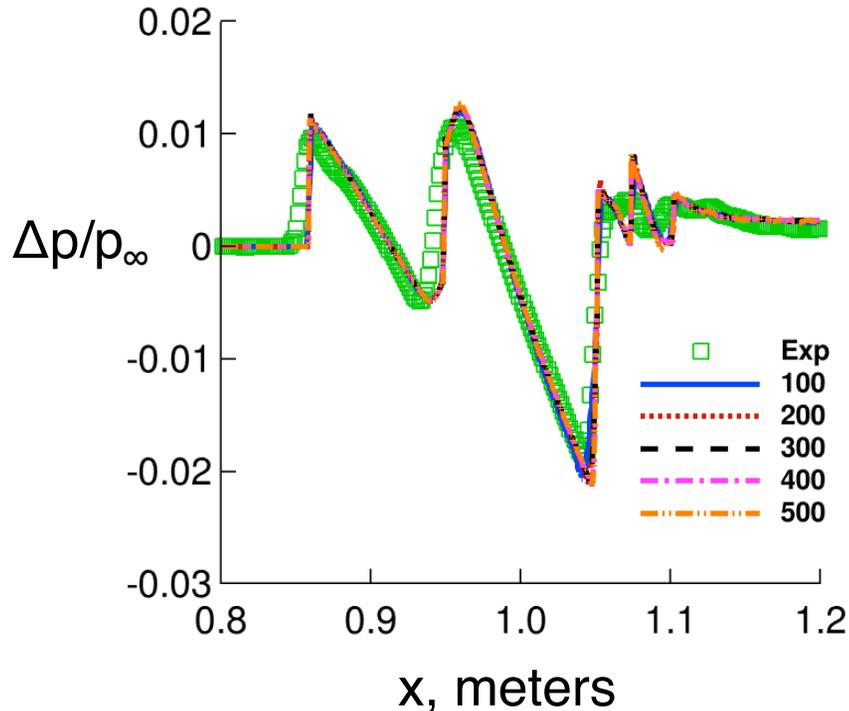


# Effect of Axial Spacing Parameter (ASP) on DWB Near-Field Boom Signature



$M = 1.7$     $H/L = 3.6$     $\Phi = 0$  deg

Grid spacing =  $L / ASP$

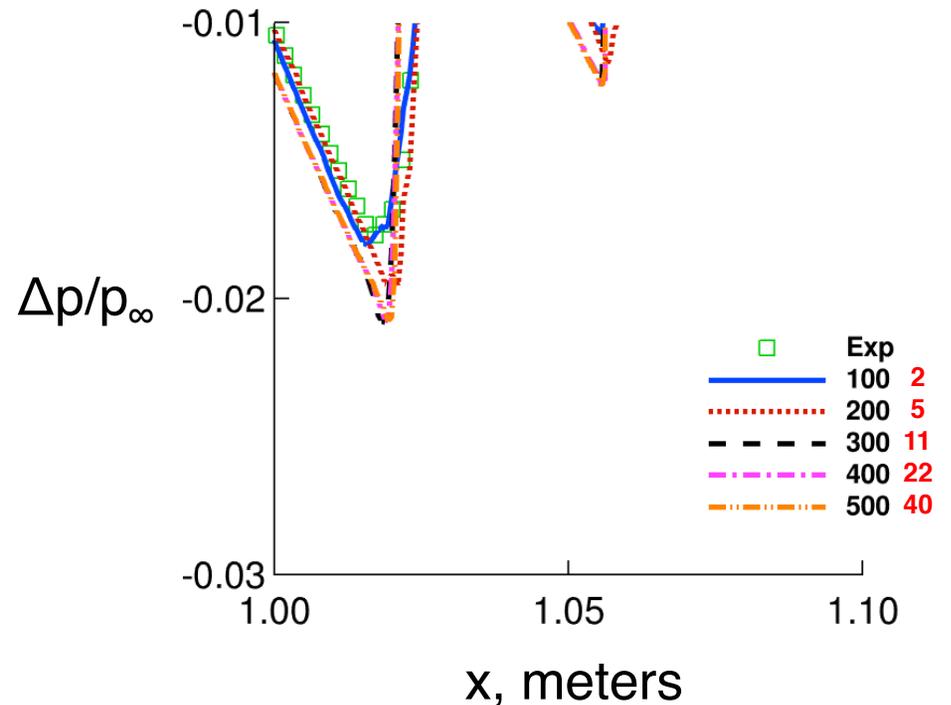
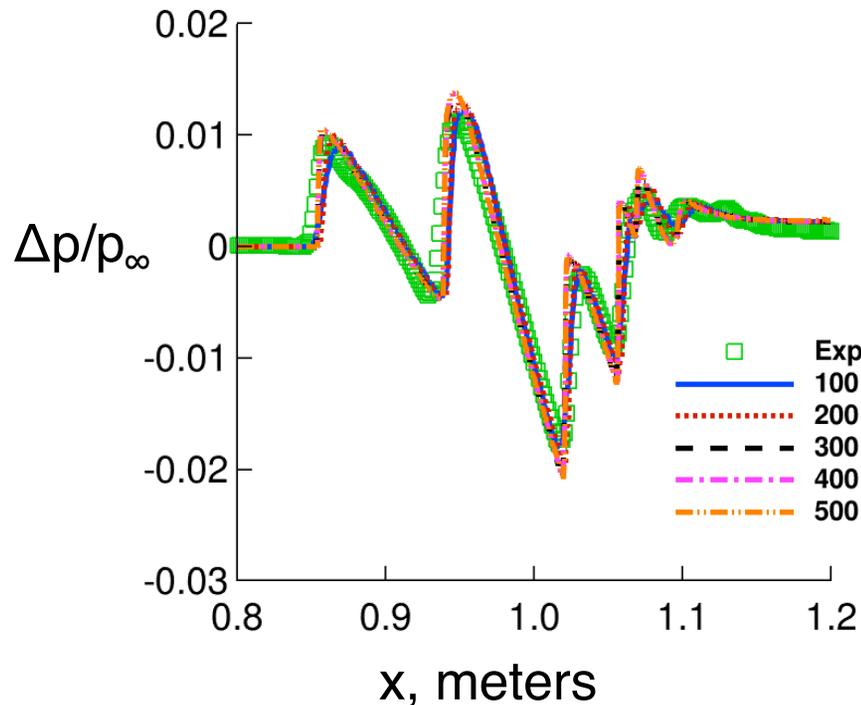


# Effect of Axial Spacing Parameter (ASP) on DWB Near-Field Boom Signature



$M = 1.7$     $H/L = 3.6$     $\Phi = 60$  deg

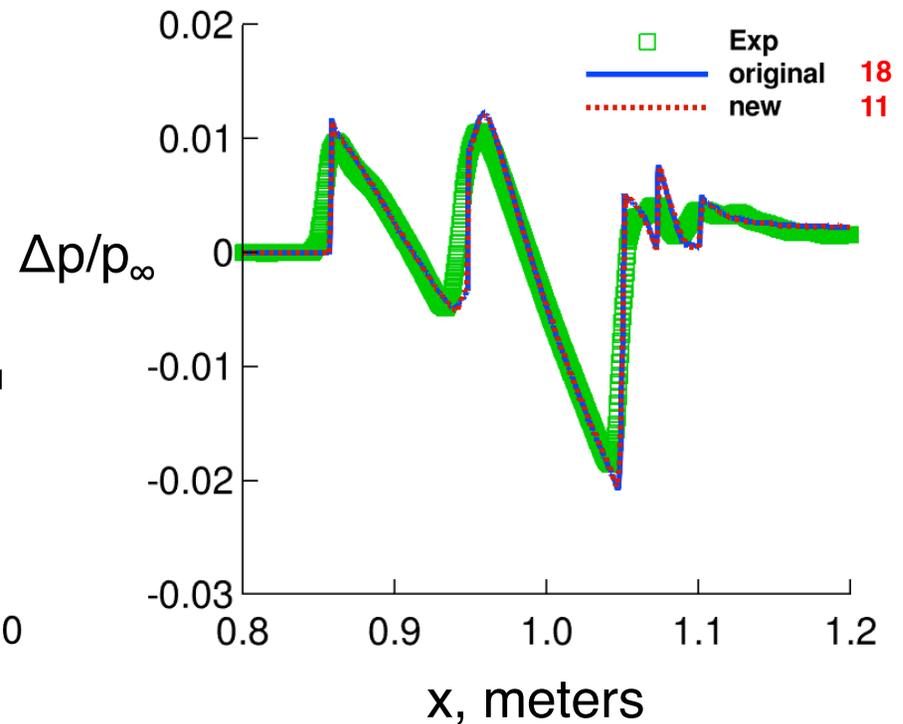
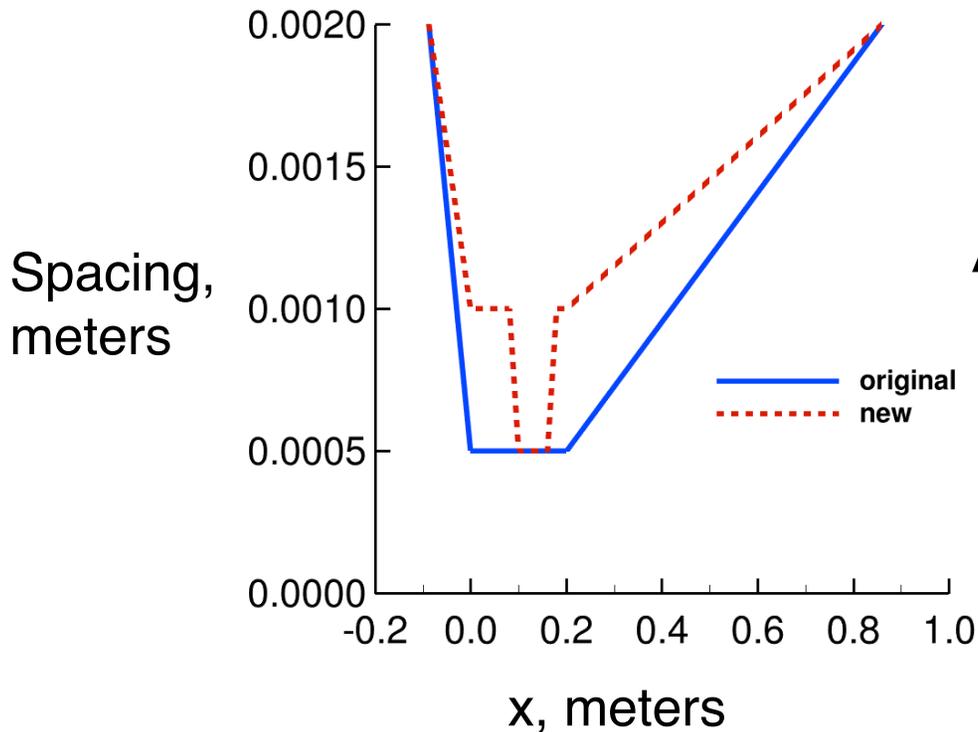
Grid spacing =  $L / ASP$



# Effect of Multi-zone Spacing Option on DWB Near-Field Boom Signature



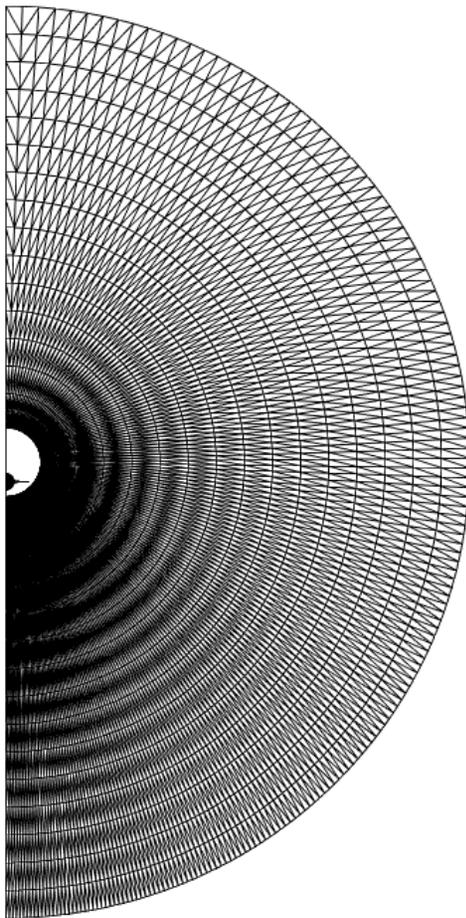
$M = 1.7$     $H/L = 3.6$     $\Phi = 0$  deg



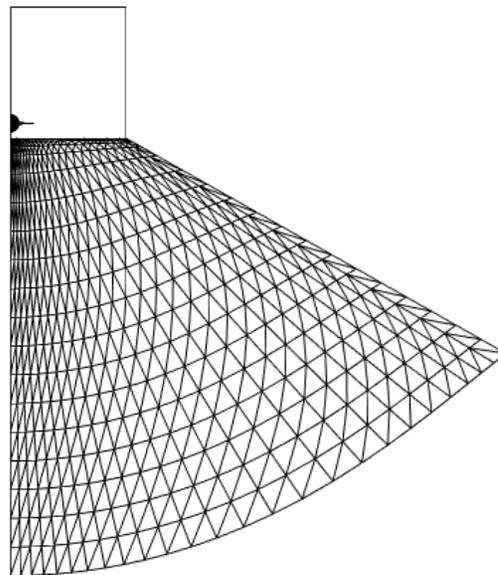
# Collar Grid Inflow Planes for Different Core Grid Outer Boundary Options



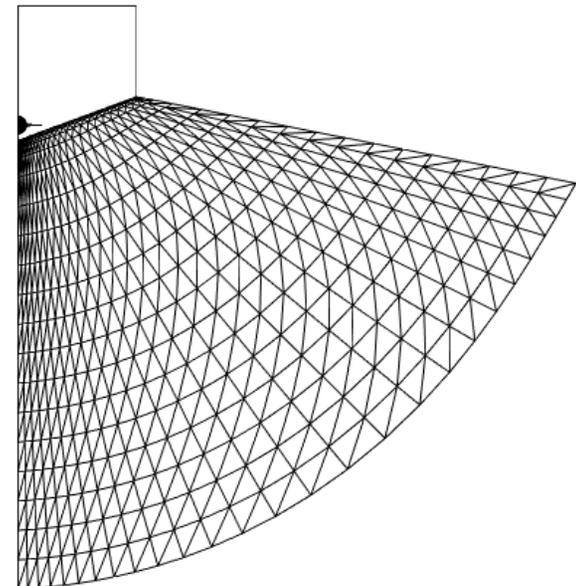
Cylindrical (COB)



Rectangular (ROB)



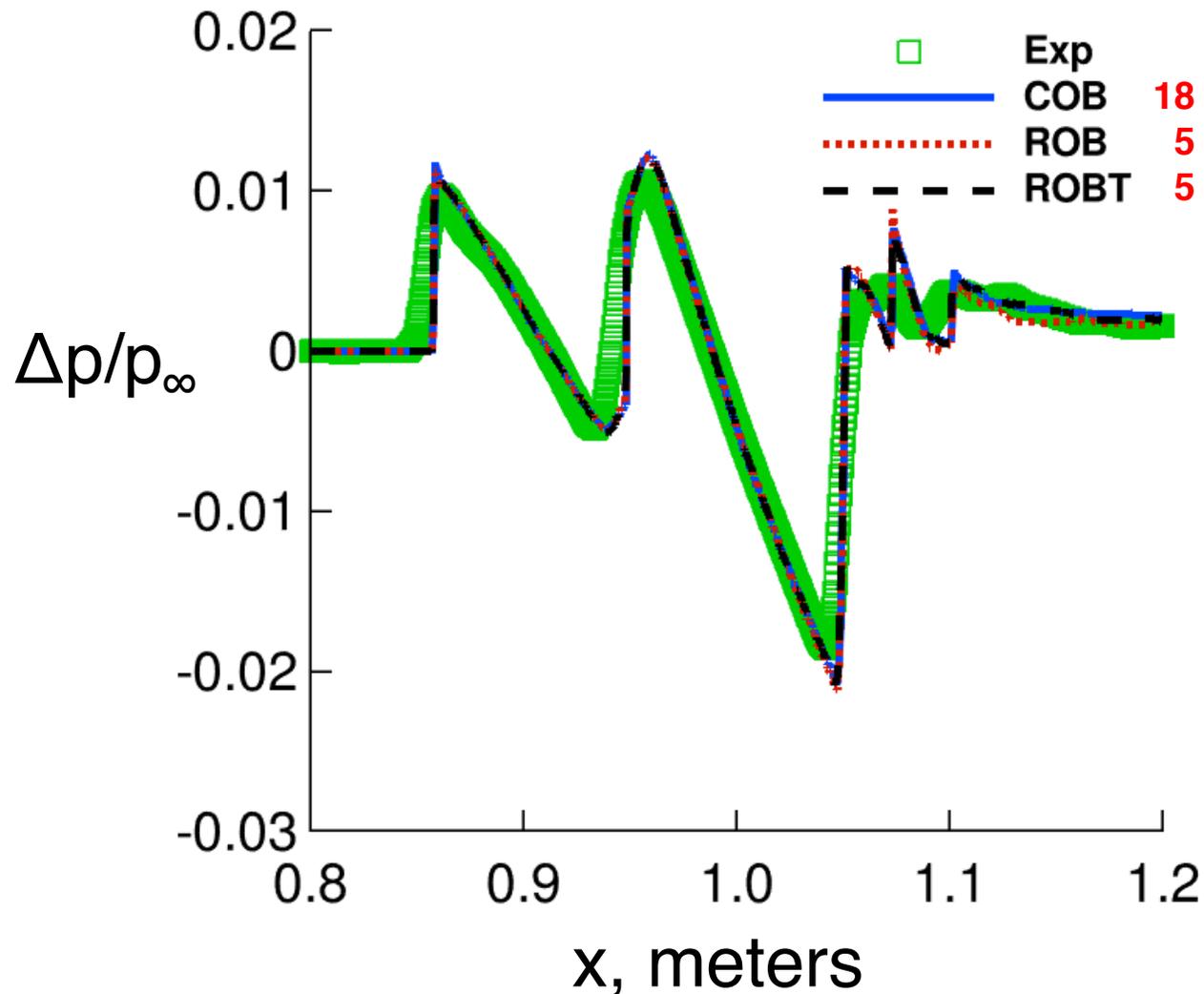
Rectangular with tilted lower boundary (ROBT)



# Effect of Core Outer Boundary Shape on DWB Near-field Boom Signature



$M = 1.7$     $H/L = 3.6$     $\Phi = 0$  deg



# Summary of Parametric Grid Generation Studies - BG

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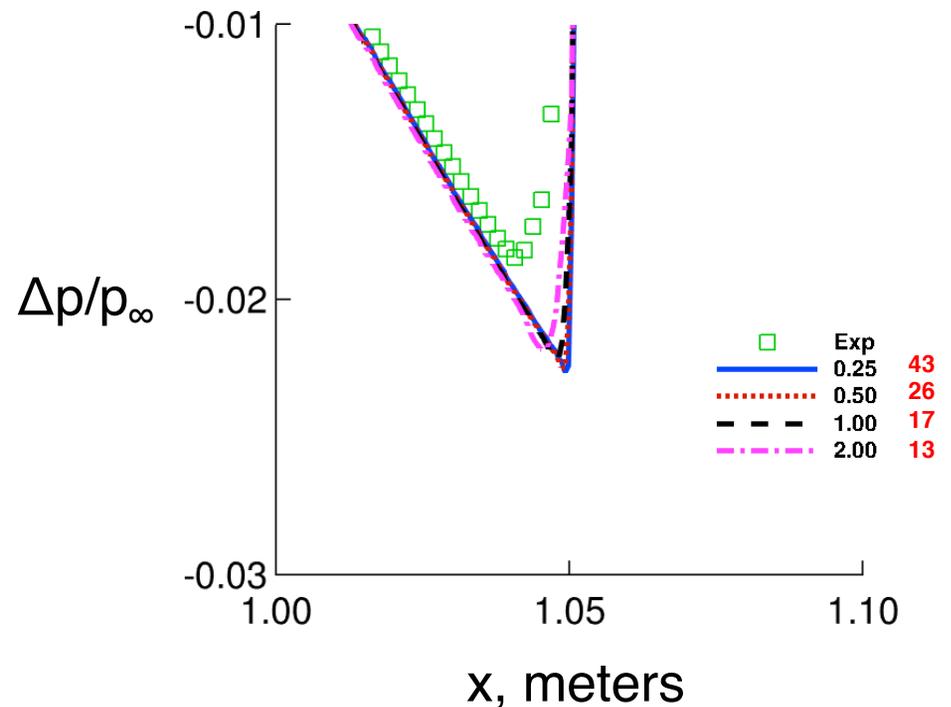
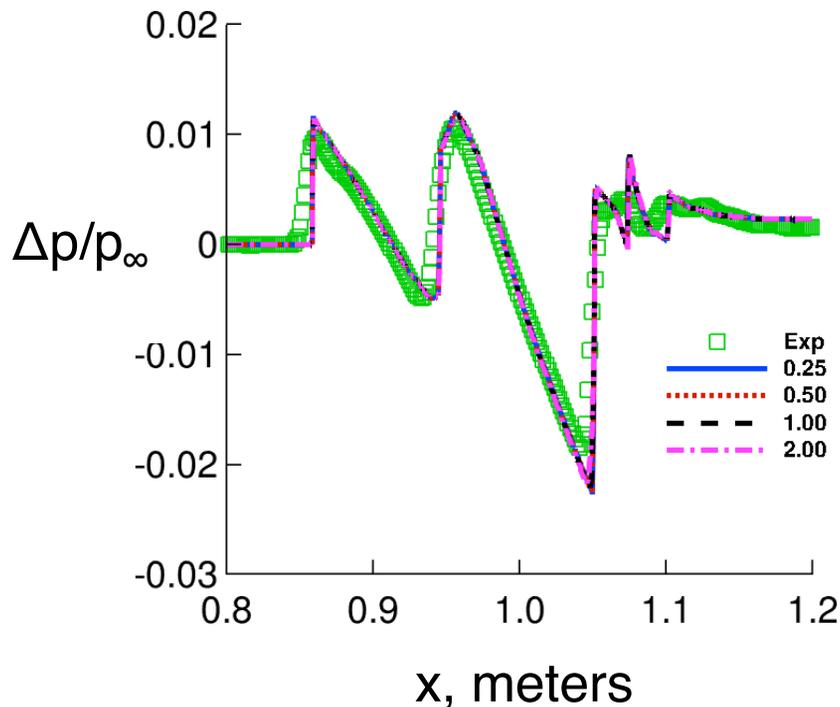


| <u>Parameter</u>        | <u>Configuration</u> | <u>Range</u> | <u>Significant</u> |
|-------------------------|----------------------|--------------|--------------------|
| Cell stretching factor  | DWB                  | 0.25 – 2.00  | yes                |
| Outer boundary distance | DWB                  | 0.0, 0.5     | no                 |
| Alpha parameter         | LM1021               | -2, 0, 2 deg | yes                |

# Effect of BG Stretching Factor (SF) on DWB Near-Field Boom Signature



$M = 1.7$     $H/L = 3.6$     $\Phi = 0$  deg

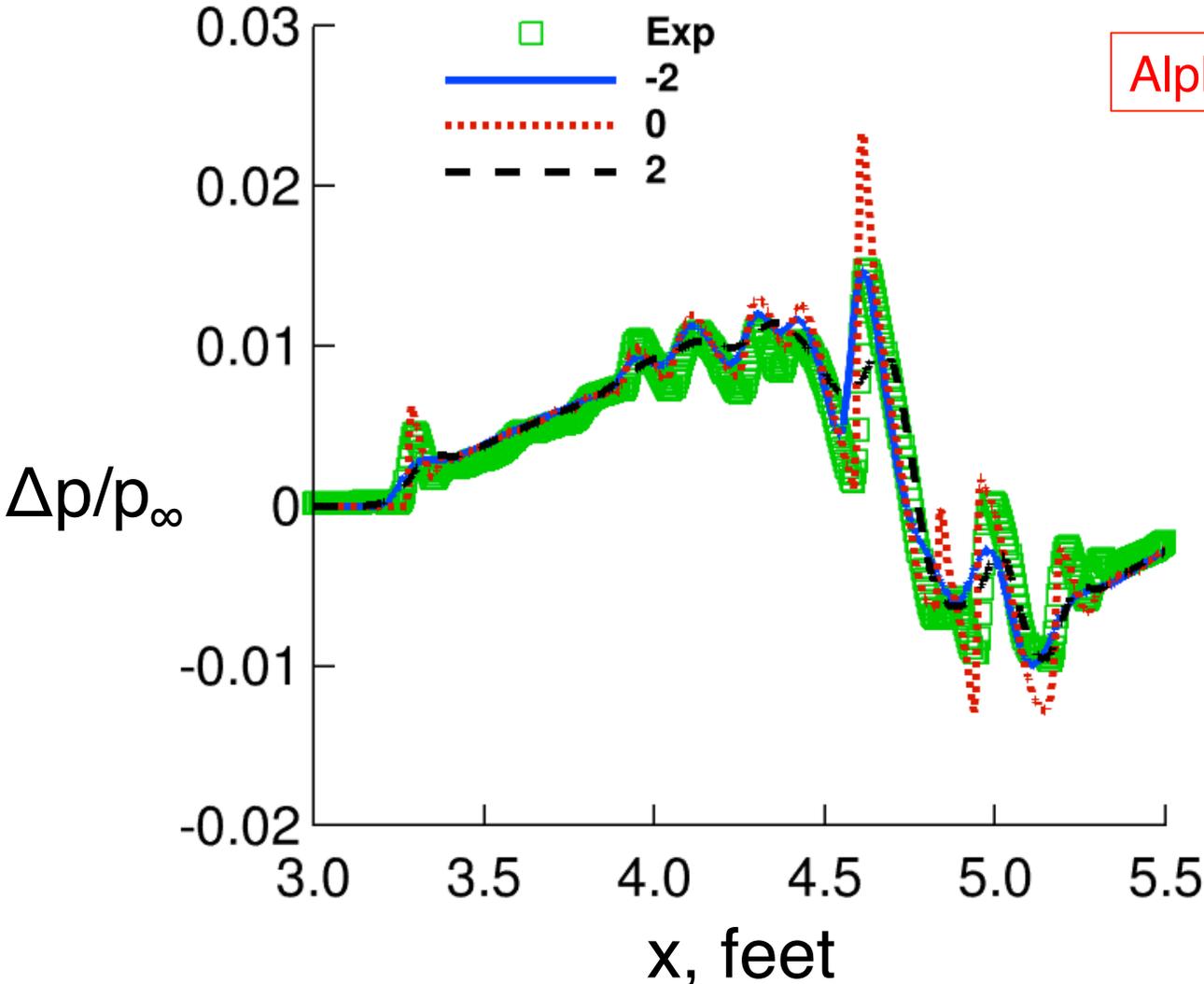


Maximum cell stretching =  $50 * SF$

# Effect of BG Alpha Parameter on LM1021 Near-field Boom Signature



$M = 1.6$     $H/L = 1.4$     $\Phi = 0$  deg



# Recommendations for Generation of Sonic Boom Grids using COB and BG

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- **COB**

- Automated vertical positioning of outer boundary
- Axial spacing =  $1/300$  of the body length
- Multi-zone option for better local resolution
- ROB option for on-track, COB if off-track is needed

- **BG**

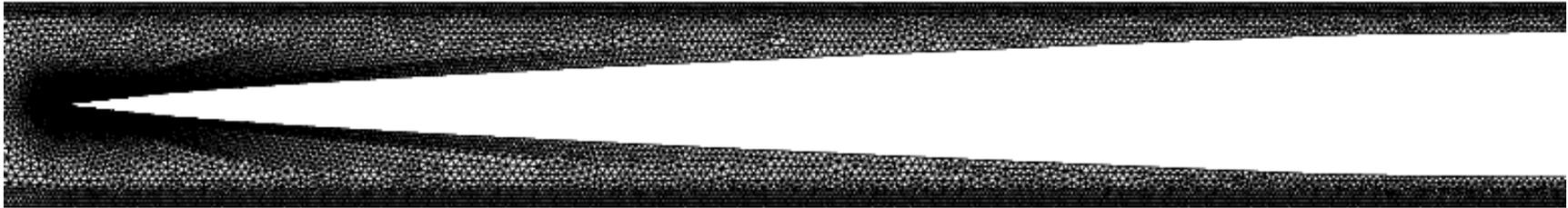
- Collar grid radial extent = signature location
- Cell stretching factor = 1.0
- Alpha parameter = flow solver angle of attack

# Core Grid Symmetry Planes for Baseline and Modified SEEB Geometry

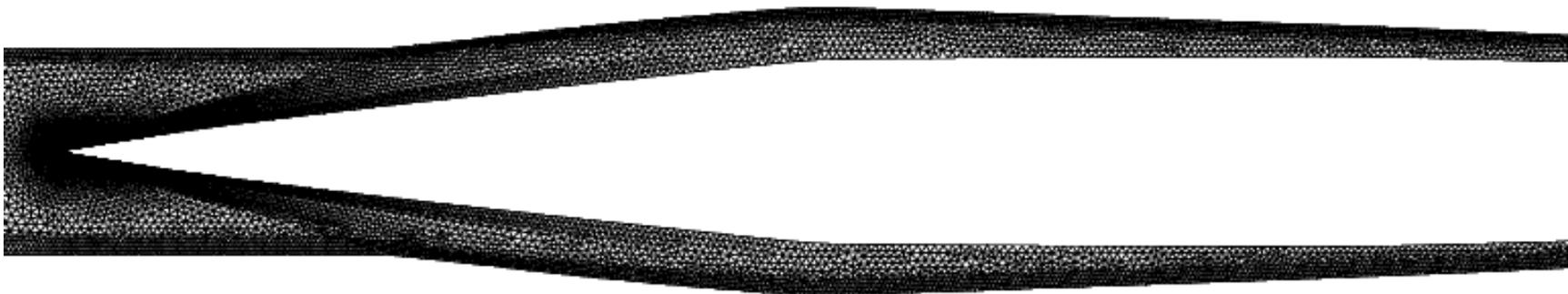
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Baseline



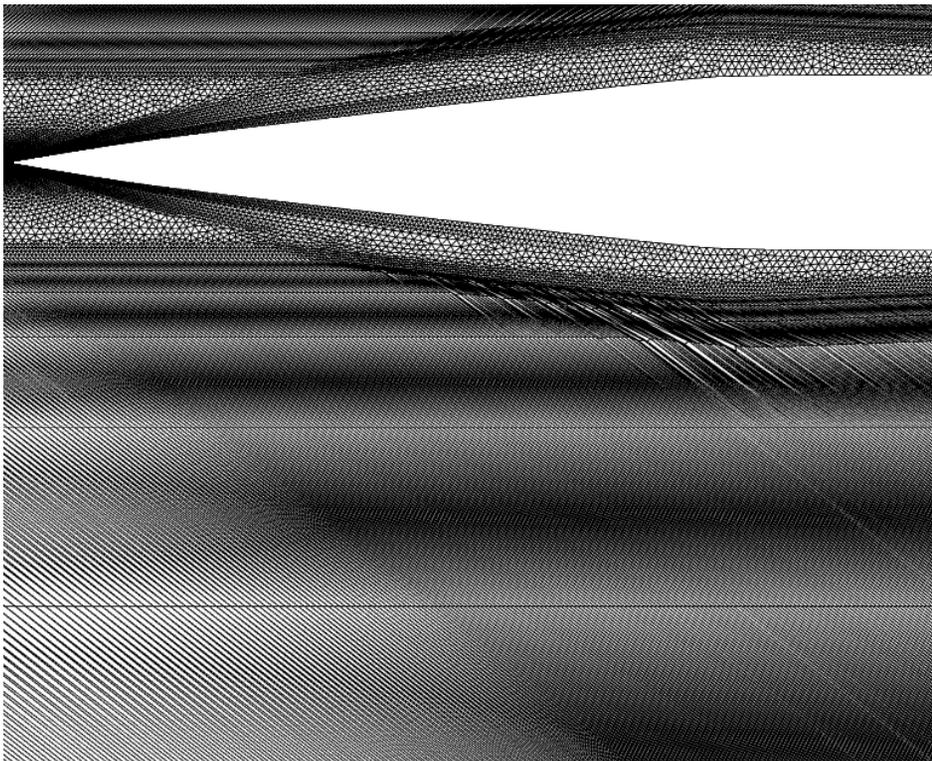
Modified



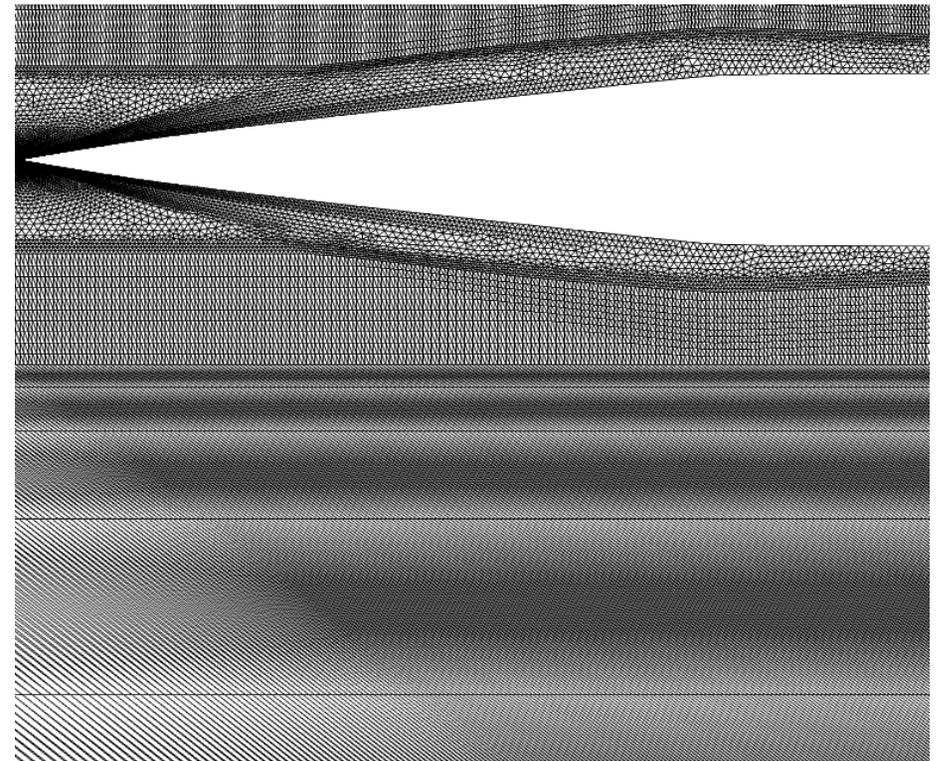
# Core Grid Symmetry Planes for Baseline and Modified SEEB Geometry



Original BG shearing



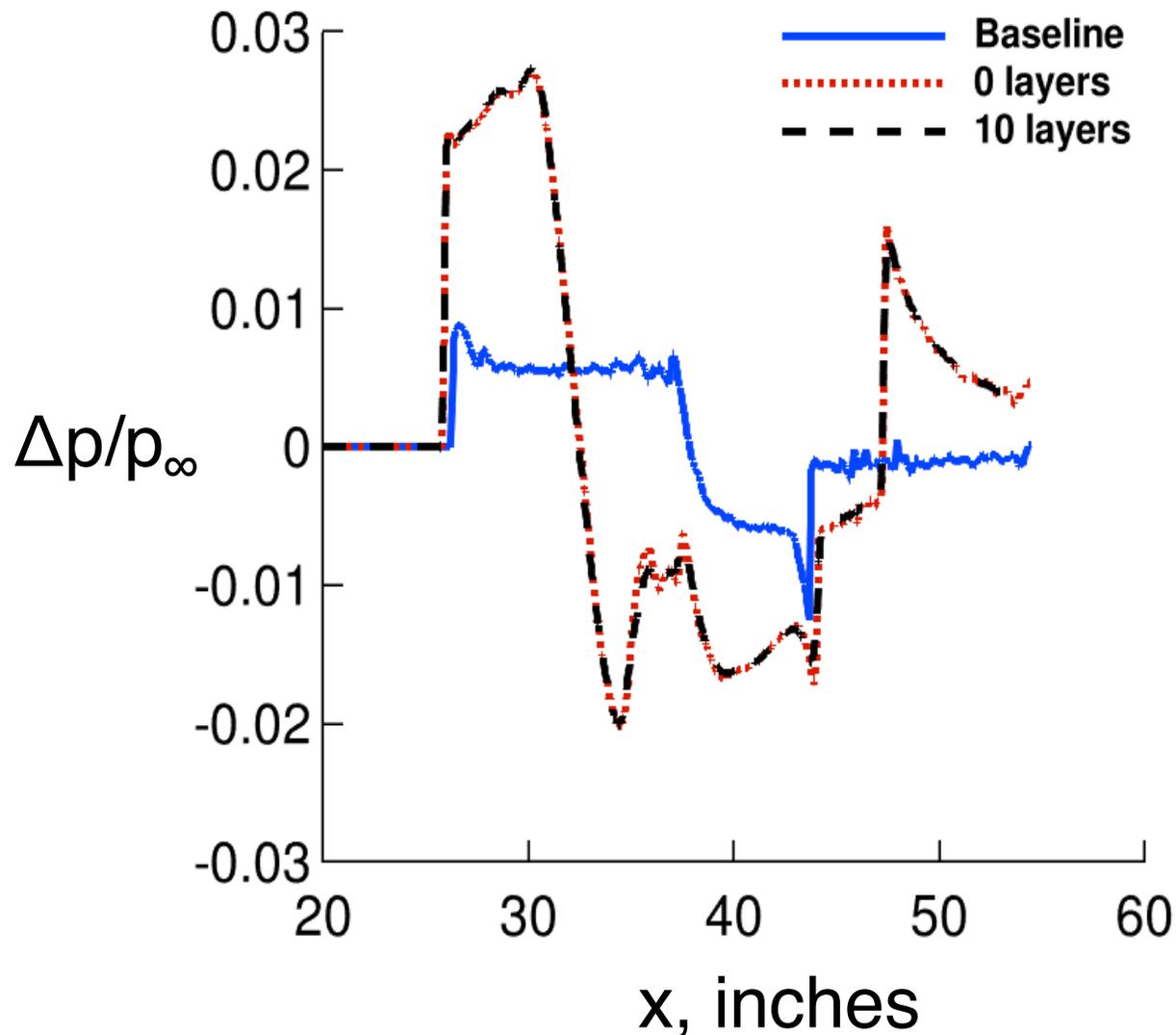
Initial uniform BG layers



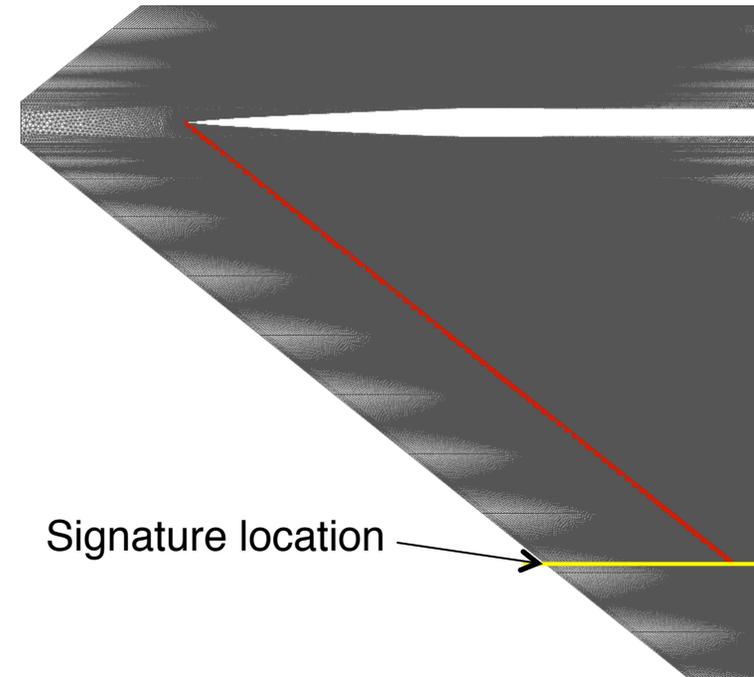
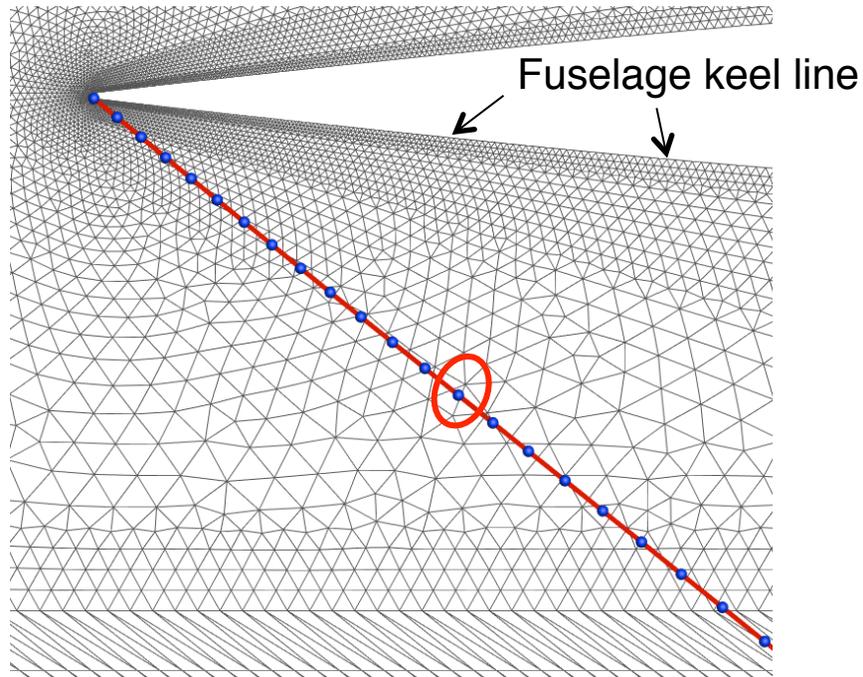
# Effect of Initial Uniform BG Layers on SEEB Near-field Boom Signature



$M = 1.6$     $H/L = 1.2$     $\Phi = 0$  deg



# NFTARG Ray-Tracing Approach to Sonic Boom Design with CDISC

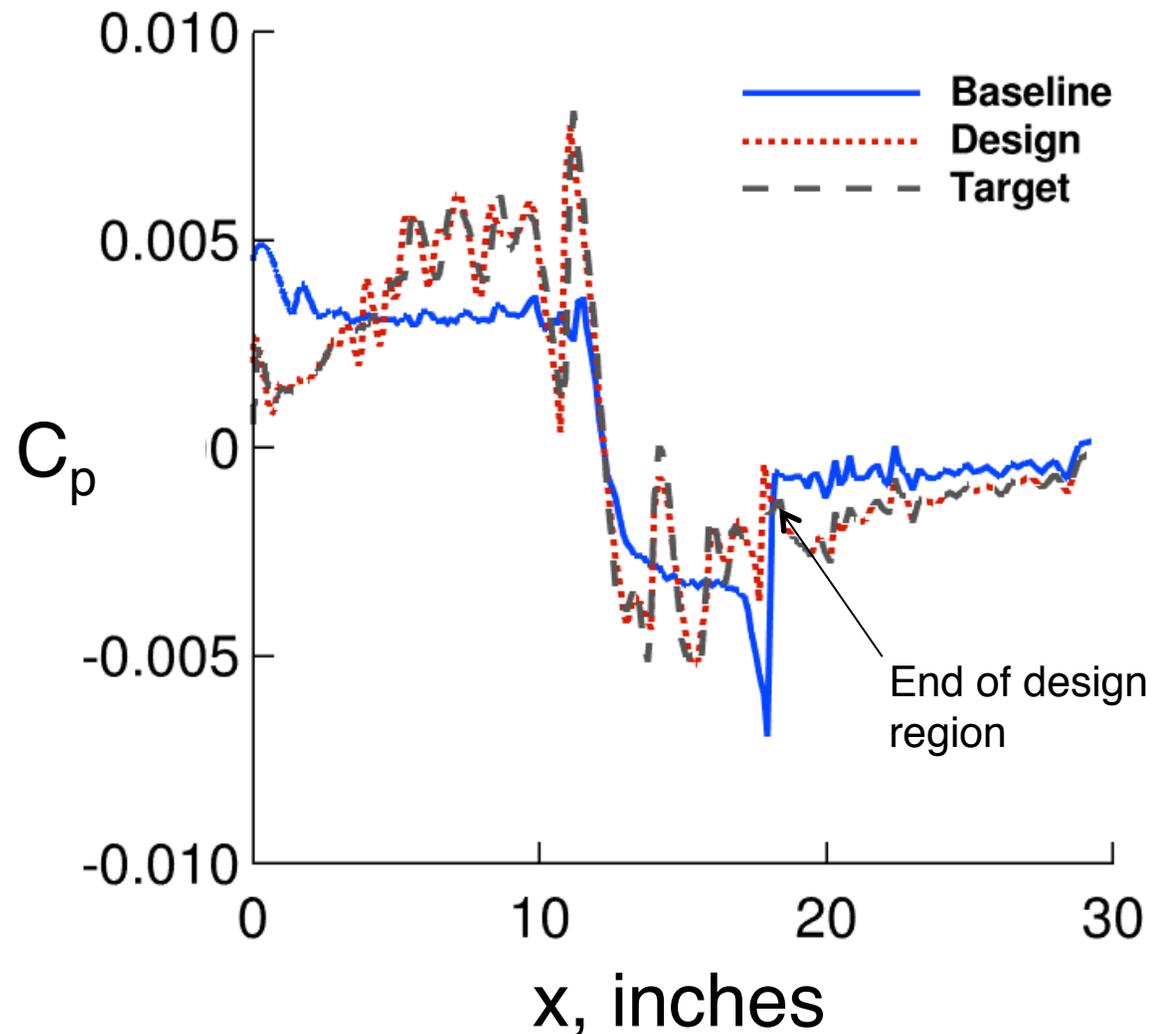


- Step from grid points on fuselage keel line to signature location
- Use Mach number from nearest grid point to determine direction for next step
- Shift beginning of signature to match ray trace from first keel point

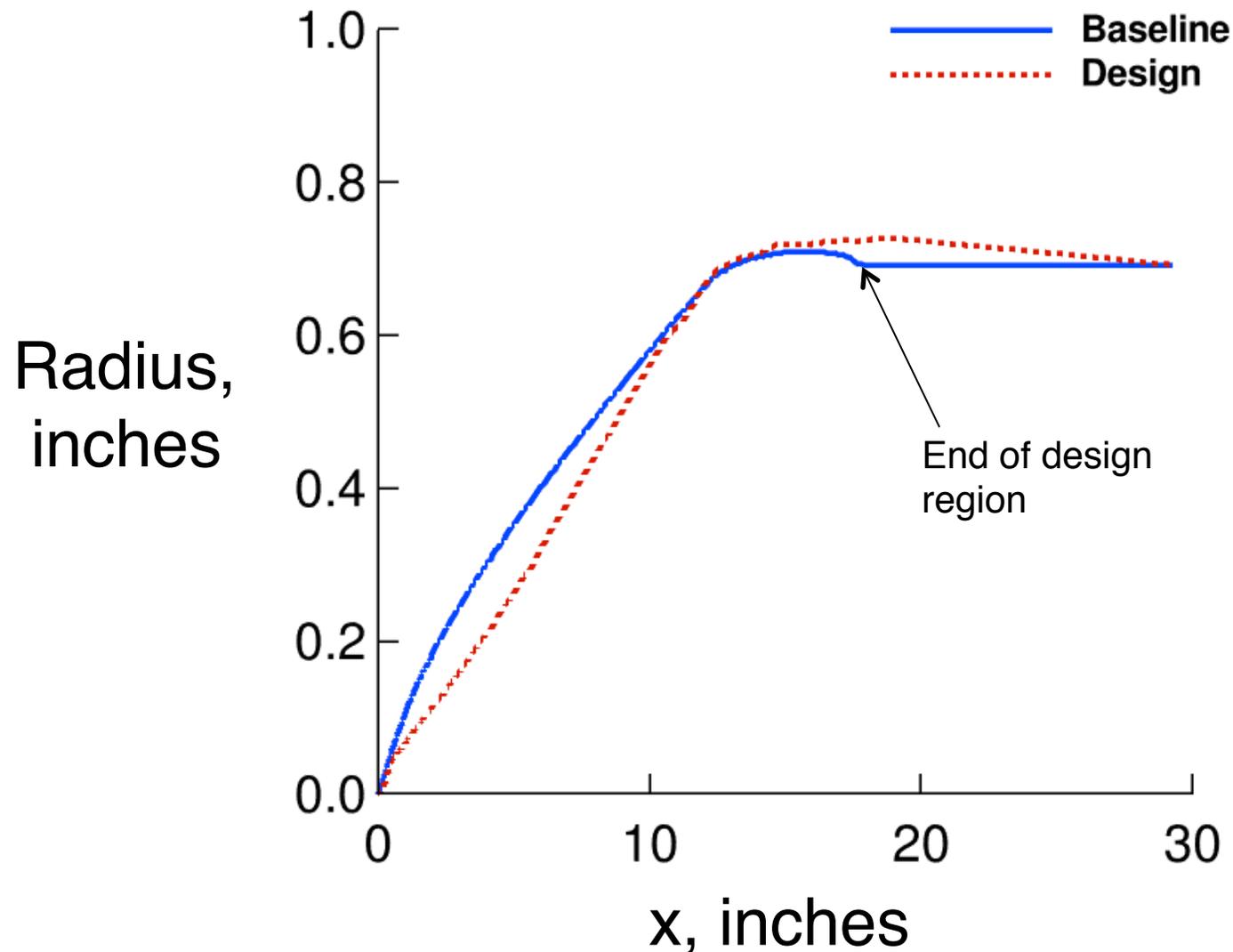
# CDISC Design of SEEB to Near-Field Signature from LM1021 - Pressures



$M = 1.6$     $H/L = 1.2$     $\phi = 0$  deg



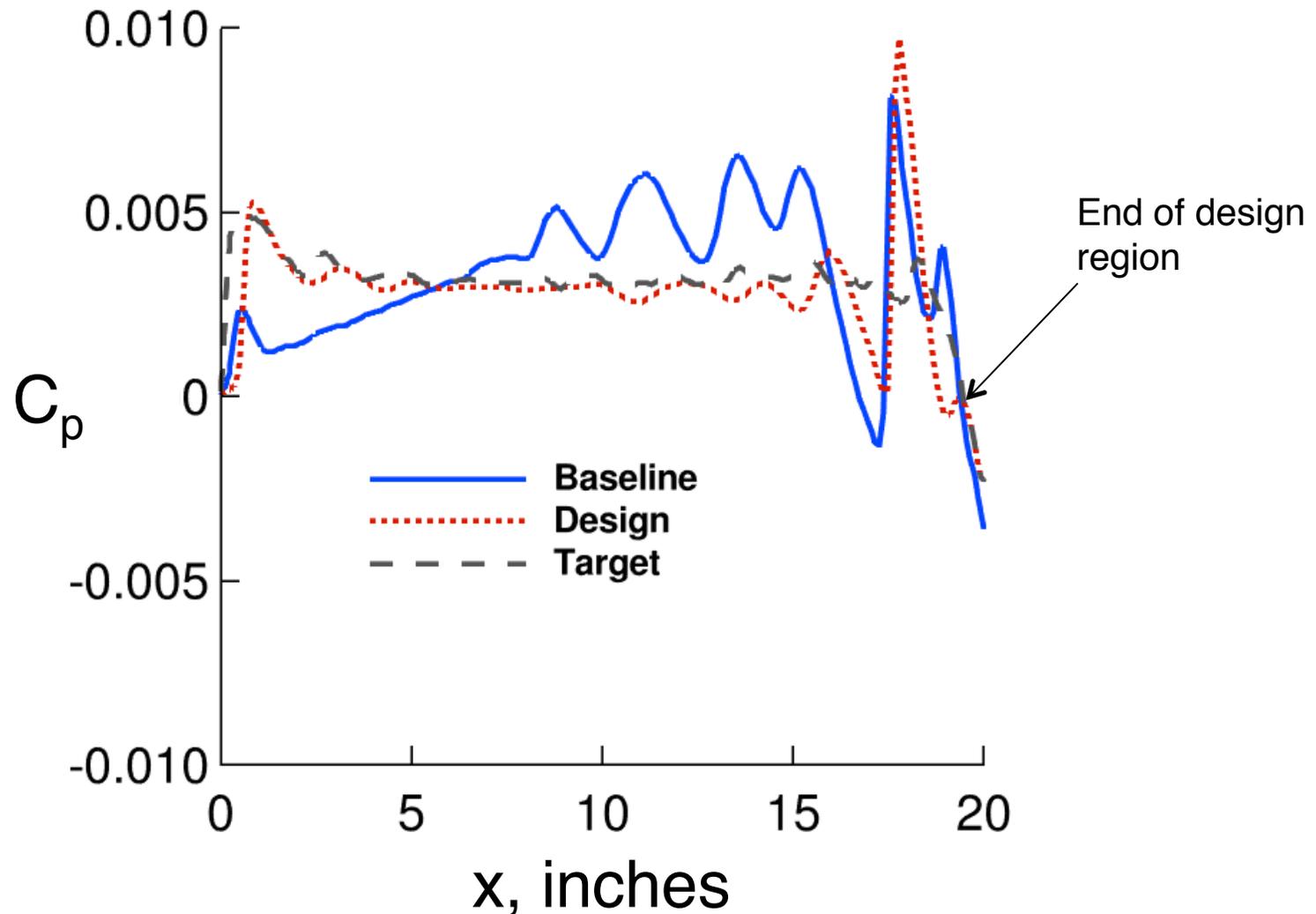
# CDISC Design of SEEB to Near-Field Signature from LM1021 - Geometry



# CDISC Design of LM1021 to Near-Field Signature from SEEB - Pressures

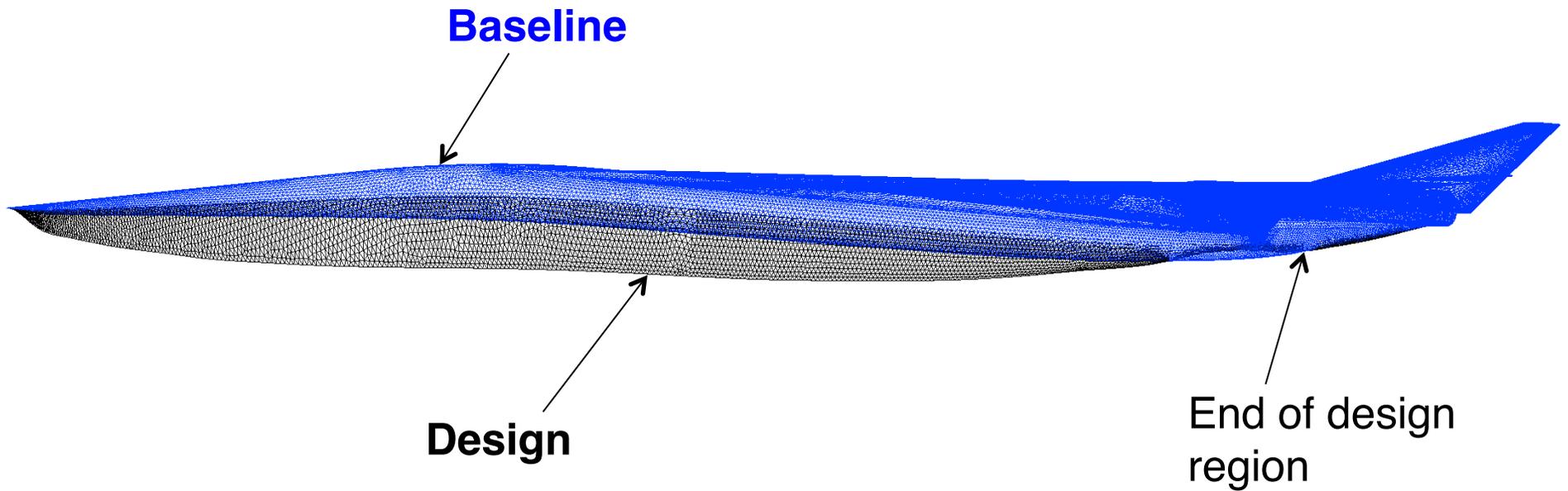


$M = 1.6$     $H/L = 1.4$     $\phi = 0$  deg



# CDISC Design of LM1021 to Near-Field Signature from SEEB - Geometry

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# Concluding Remarks

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- COB and BG generally produced similar boom signatures across the range for parameters investigated
- Initial guidelines for COB and BG input parameters have been suggested
- CDISC with NFTARG was effective for designing to a target near-field boom signature
- Boom design requires 2-5x more flow iterations per design cycle than the traditional CDISC surface pressure design